

22ND ACERC Conference
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REFRACTORY-SLAG INTERACTIONS IN COAL GASIFICATION ENVIRONMENTS

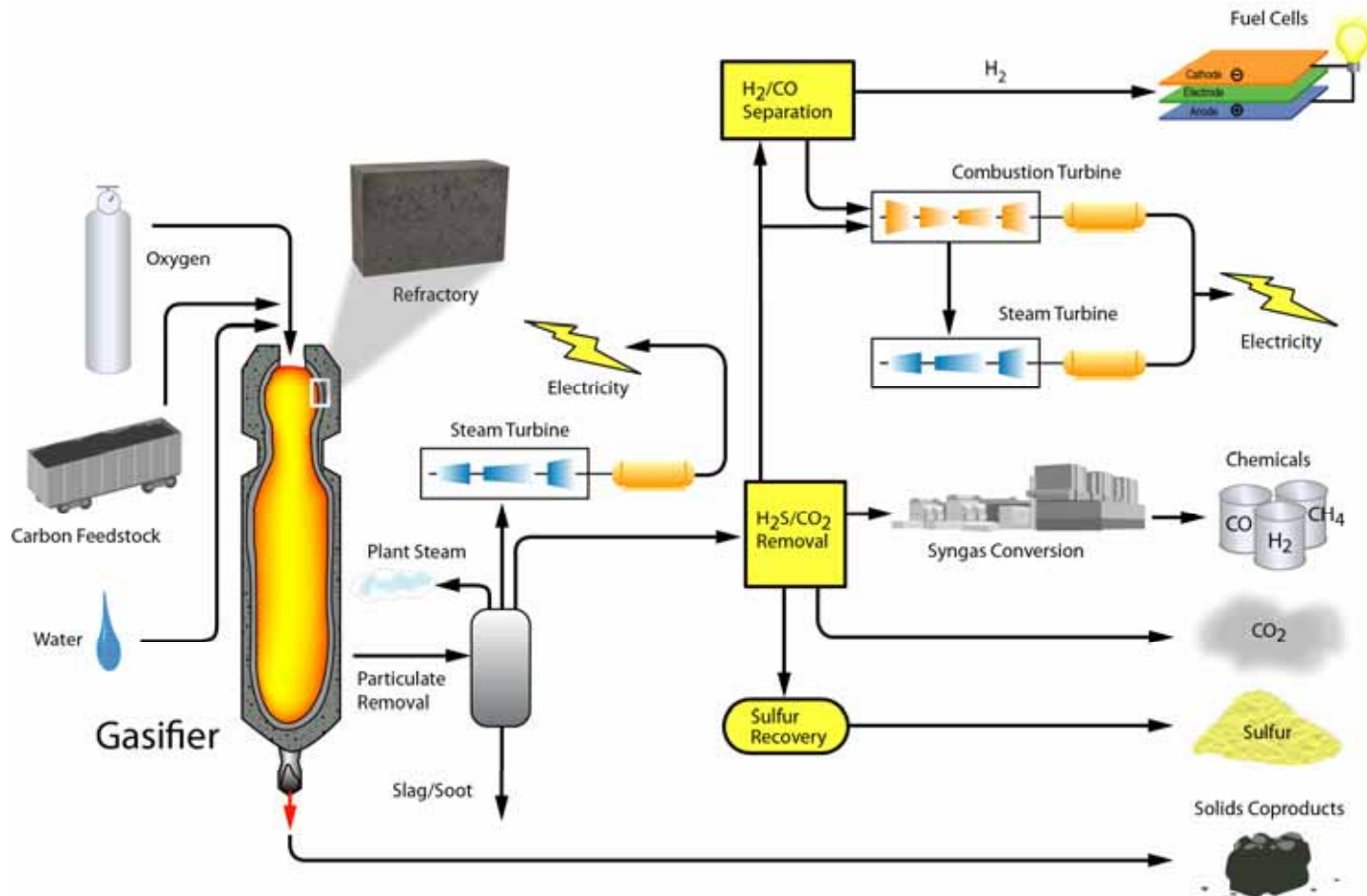
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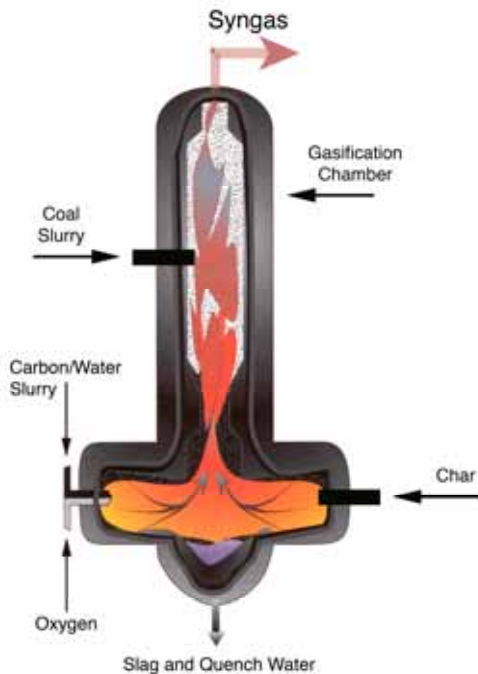
Gasification Background



Gasification Reaction



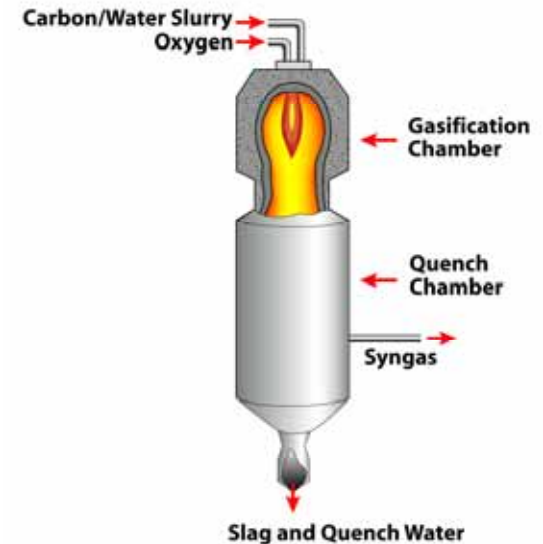
Material Challenges Inherent to Air-cooled Slagging Gasifiers



ConocoPhillips

(2 stage - syngas cooler)

- Operating temperatures of 1325° to 1575°C
- Thermal cycling
- Reducing and oxidizing environment
- Corrosive slags of variable chemistry (*slags from minerals in carbon feedstock*)
- Corrosive gases
- Pressures ≥ 400 psi



GE Design

(1 stage - syngas cooler or water quench)

Refractory Material Issues - Consequences

1. Low system reliability, on-line availability

- gasifier down as frequently as once/month
- possible need for “spare” gasifier

2. Lost opportunity costs

3. Frequent maintenance/high costs

4. Need for zoning – larger “spare” material inventory

5. High material repair costs

- \$1 million for refractory lining
- long downtime for repairs

6. Excessive safety margins



Gasifier Program Goals

- **Increased reliability and availability**
 - 85-95% for power generation, 90% for chemical production
 - Service life of 3 + years in power generation
- **Carbon feedstock flexibility, including biomass**



Range of Chemistry Found in Over 300 U.S. Coal Slags Due to Mineral Impurities

<u>Material</u>	<u>Weight Percent</u>			
	<u>Max.</u>	<u>Min.</u>	<u>Avg.</u>	<u>Std. dev.</u>
SiO₂	68.5	7.1	43.6	16.4
Al₂O₃	38.6	4.1	25.2	10.2
Fe₂O₃	69.7	2.1	17.0	11.2
CaO	45.1	0.5	5.8	6.6
MgO	8.0	0.1	1.2	1.1
K₂O	3.5	0.2	1.4	0.7
Na₂O	6.5	0.3	0.9	0.6
TiO₂	3.7	0.4	1.4	0.8

Source: W.A. Selvig and F.H. Gibson; Analysis of Ash from United States Coals; USBM Bulletin, Pub. 567; 1956, 33 pp.

Note: Petcoke slags contain V and Ni

Chemical Composition* of High Cr₂O₃ Gasifier Refractories

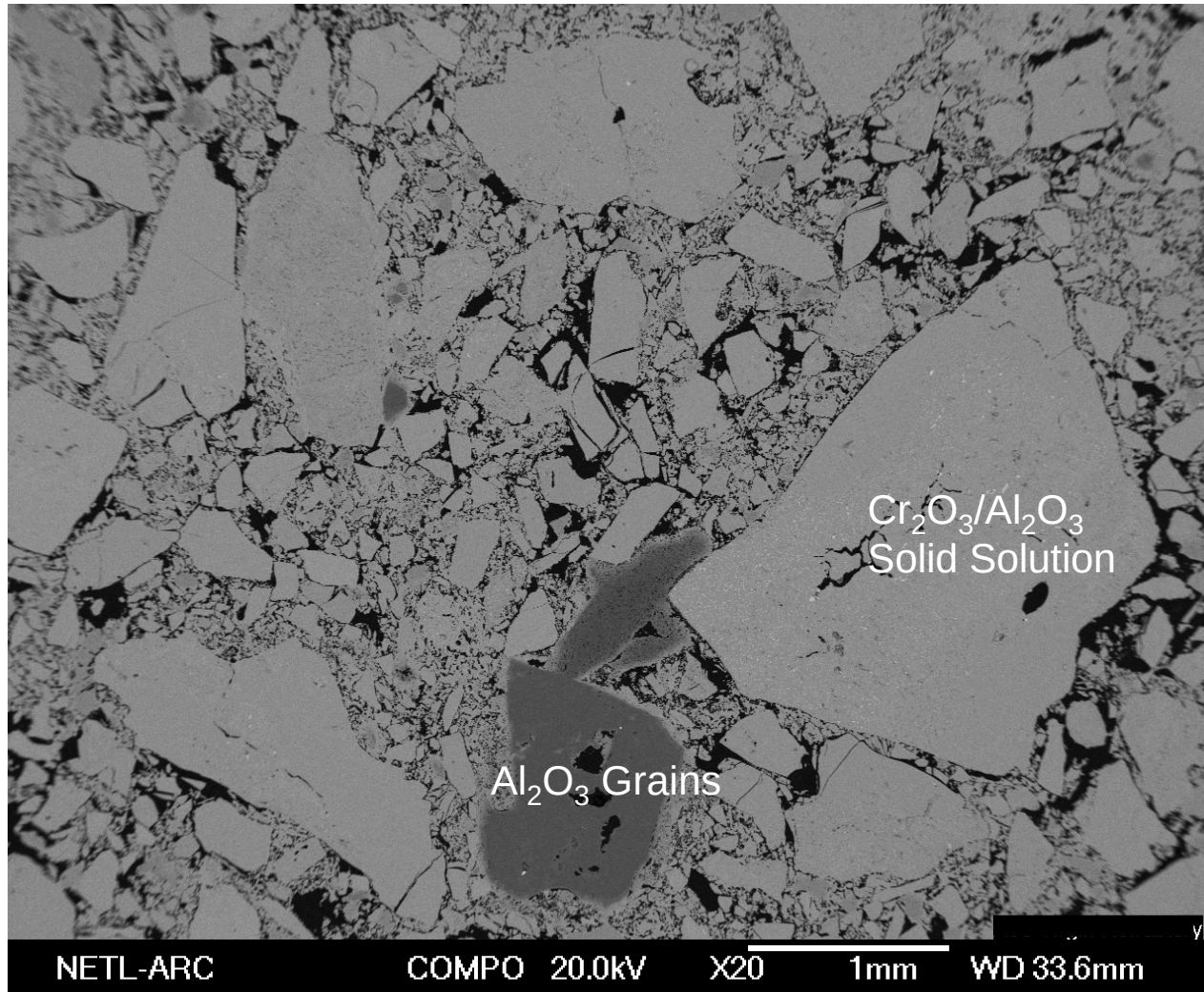
	<u>Composition</u>		
<u>Chemistry</u>	<u>A</u>	<u>B</u>	<u>C</u>
Cr ₂ O ₃	89.0	87	92.0
Al ₂ O ₃	10.2	3.0	4.7
ZrO ₂	---	6.5	---
P ₂ O ₅	---	---	3.3
<u>Bulk Density (g/cc)</u>	4.21	4.07	4.23
<u>Porosity (pct)</u>	16.7	16.5	15.0
<u>CCS (MPa)</u>	48.3	66.9	51.7

NETL developed,
patented material

Conventional materials

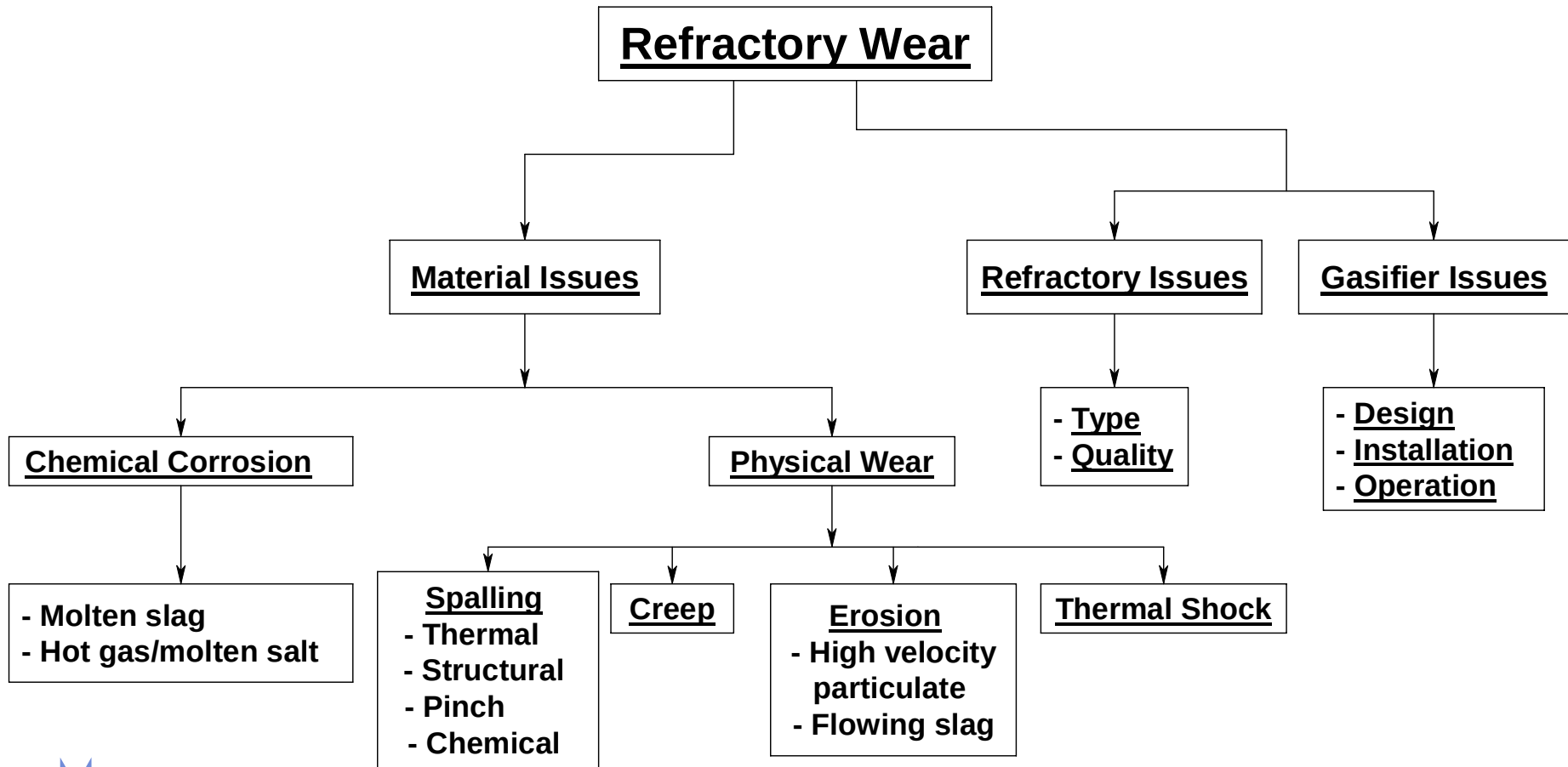
* = Information from product data sheet

Typical Virgin Commercial Refractory Microstructure

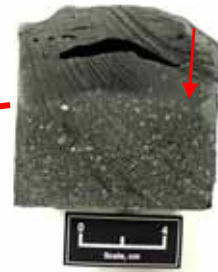


Cause of Refractory Wear

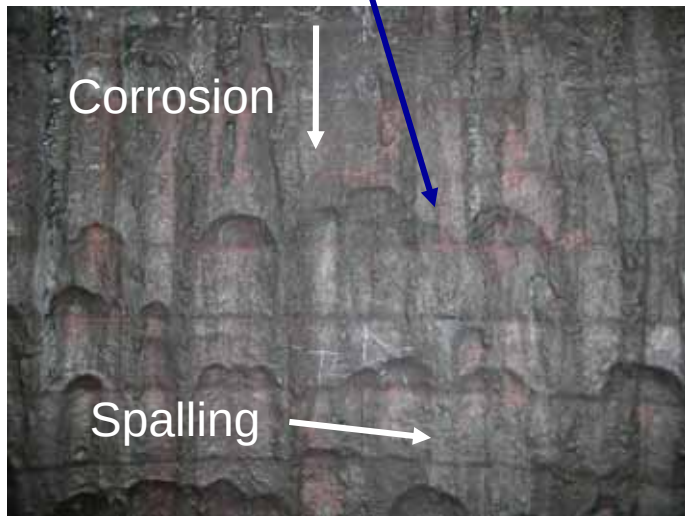
(High Cr_2O_3 Materials)



Material Challenges Inherent to Air-cooled Slagging Gasifiers



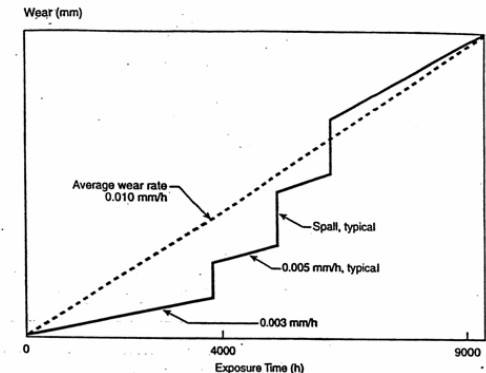
Slag
penetration



High chrome oxide liners
(60-95 pct Cr_2O_3)

- Operating temperatures of 1325° to 1575°C
- Thermal cycling
- Reducing and oxidizing environment
- Corrosive slags of variable chemistry (*slags from minerals in carbon feedstock*)
- Corrosive gases
- Pressures ≥ 400 psi

Spalling



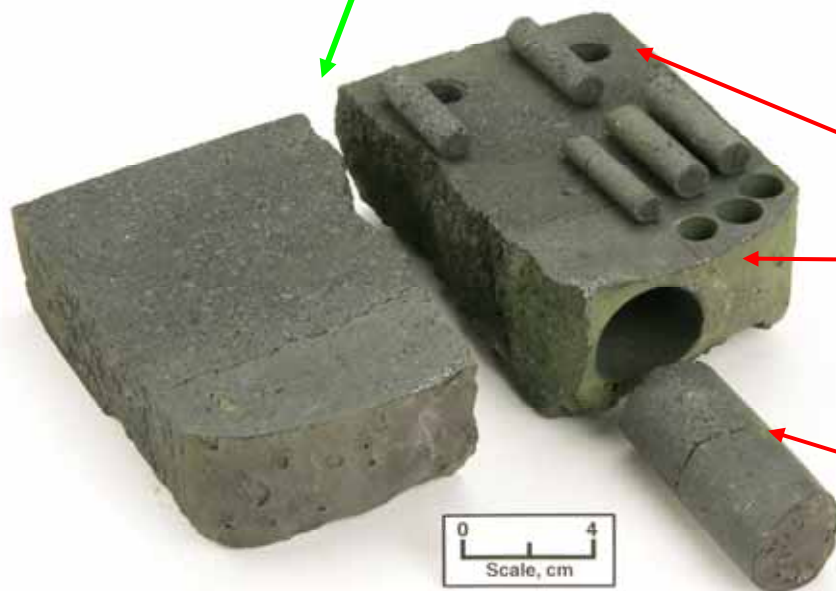
Combined Wear

W.T. Bakker, "Refractories for Present and Future Electric Power Plants," Key Engineering Materials, Trans Tech Publications, (1993), Vol. 88, pp. 41-70.



Post-Mortem Analysis

(Commercial Refractory $\approx$ 180 days of exposure to coal slag from 1350-1450°C)



Thermal Expansion Cores

Cold face: 7.68×10^{-6} mm/mm/°C

Hot face: 8.18×10^{-6} mm/mm/°C

Chemical, X-Ray Crystalline Phases, Microstructure

Chemistry of High Chromia Commercial Refractory Versus Depth from Hot Face

Distance from Hot Face (mm)	Bulk Chemistry (wt pct)					X-Ray Crystalline Phases
	Cr ₂ O ₃	Al ₂ O ₃	SiO ₂	CaO	Fe	
H.F. to 2.3	80.0	10.8	5.4	0.3	1.6	P= Cr ₂ O ₃ Tr=M*Cr ₂ O ₄
6.9	84.2	10.2	3.9	0.3	0.4	P= Cr ₂ O ₃ Tr=M*Cr ₂ O ₄
11.4	83.9	10.7	3.2	0.4	0.4	P= Cr ₂ O ₃ Tr=M*Cr ₂ O ₄
34.3	83.5	10.4	2.8	0.6	0.4	P= Cr ₂ O ₃
43.3	83.9	9.3	2.3	0.5	0.2	P= Cr ₂ O ₃
52.7	85.7	10.5	0.9	0.2	0.2	P= Cr ₂ O ₃
57.2	86.1	10.5	0.2	0.0	0.2	P= Cr ₂ O ₃
127	87.4	9.4	0.2	0.2	0.2	P= Cr ₂ O ₃

M = (Fe, Mg, Ni, ...) solid solution

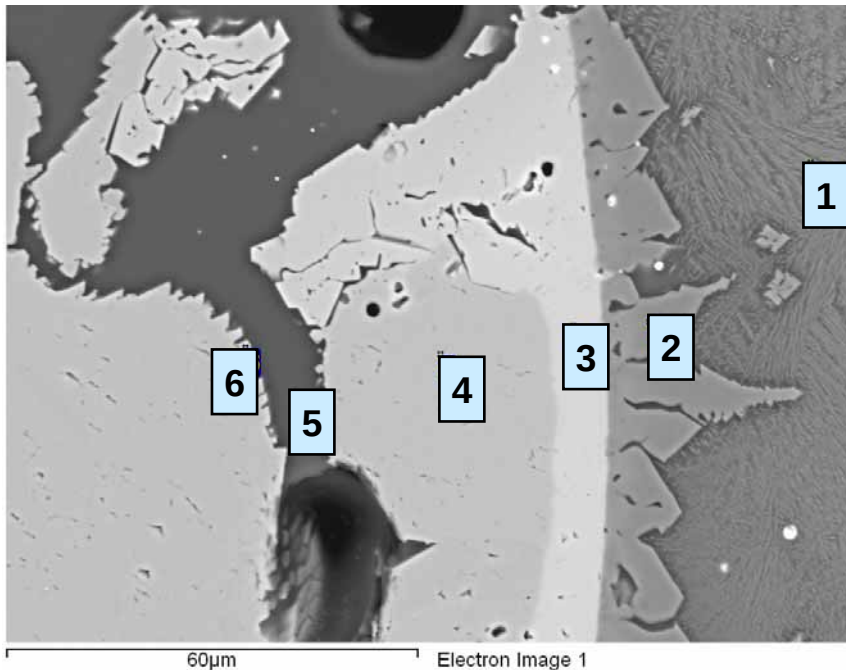
M*Cr₂O₄ = spinel

Point Chemistry

<u>Chemistry</u> (weight %)	<u>Point</u>					
	<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>	<u>5</u>	<u>6</u>
- Al	6.9	27.3	1.7	2.8	7.5	5.7
- Si	23.9	0.2	0.1	0.1	40.2	3.8
- Fe	20.8	31.7	23.6	0.2	1.5	0.5
- Ca	1.5	-	-	-	0.5	-
- Cr	0.1	1.5	42.7	62.1	1.5	53.0

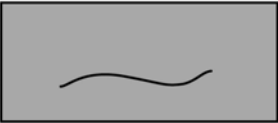
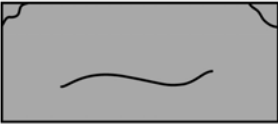
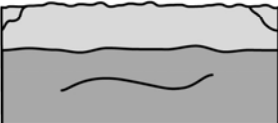
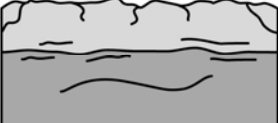
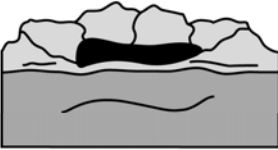
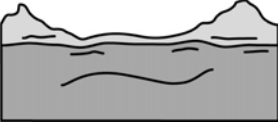
<u>Point</u>	<u>Crystalline phases</u>
1	Hercynite, Fayalite, Enstatite, Iron sulfide, Iron cordierite, Hermatite
2	Iron-alumina spinel
3	Iron-chrome spinel
4	Chromia/alumina solid solution
5	Fe depleted slag
6	Al build-up with Si

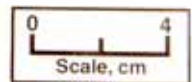
Possible Crystalline Phases



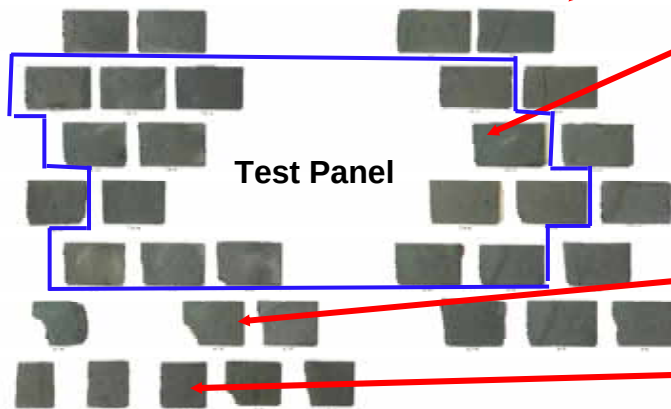
**SEM Micrograph of the
Slag/Refractory Interface
After ≈ 85 Days of Exposure
to a Coal Slag at 1400-1500°C**

Corrosion and Spalling Wear

Stage	Sample	Description
1		New Refractory may contain internal cracks from pressing, firing.
2		Preheat Pinch spalling due to hoop stresses
3		Infiltration, Corrosion - Molten slag infiltration on hot face, cracks and pores. - Surface corrosion due to slag begins
4		Horizontal Crack Formation <i>due to:</i> - Thermal cycling - Stresss accumulation - Creep
5		Void Formation - Cracks join - Internal void formation - Spalling (peeling) begins - Creep occurs on slag penetrated hot face - Hot face corrosion continues
6		Renewed Cycle - Material breakoff on hot face - Steps 3-5 repeat



Internal Flaws – Improved Versus Conventional Cr₂O₃ Refractory *(sidewall test panel – 237 days)*

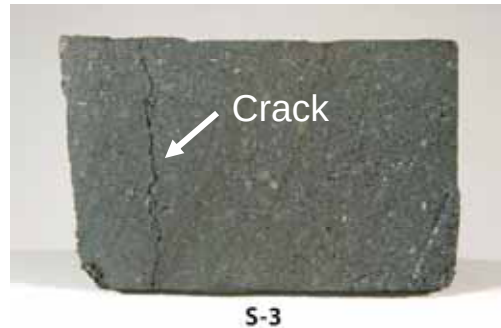


Cross Section of Brick in Test Panel

Impact of Phos on Slag Penetration, Corrosion

Conventional

1. No evidence of spalling in phosphate modified refractory



2. Reduced slag penetration

25-45 mm depth

3. Microstructure

Higher porosity

Phosphate Modified



Preliminary indication, 3-5 mm depth

Slag forms dense Fe/Cr spinel layer, higher viscosity slag, better thermal shock

Conclusions

- Slag interacts with the refractory causing wear by two means, chemical corrosion and spalling
- Microstructure changes occurring on the surface are primarily:
 - a $\text{Cr}_2\text{O}_3/\text{FeO}$ spinel that forms on the hot face refractory surface, increasing slag viscosity, slowing slag penetration
 - a high alumina layer is formed on the hot face surface. The origin of the Al_2O_3 is not clear
- Slag infiltrates into the porous refractory, causing differences in material properties between the penetrated/non penetrated layers, leading to structural spalling.
- Phosphate additions to the refractory microstructure decrease spalling wear.