Turbulent Reacting Flow Modeling of Solid Propellant Rocket Motors

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ATK Thiokol



An advanced space and weapon systems company



Actively Involved in Improved Environment Modeling Approaches for Solid Propellant Rocket Motors

- Review published approach, based on comprehensive CFD modeling. (Sabnis, J.S., "Numerical Simulation of Distributed Combustion in Solid Rocket Motors with Metalized Propellant," Journal of Propulsion & Power, Vol. 19, No. 1, 2003)
- Details of current areas of development cannot be shared because of ITAR restrictions



OUTLINE

- Overview of rocket motor flowfield
- Propellant Surface Combustion
- Multi-phase, turbulent fluid dynamics
- Aluminum droplet combustion
- Droplet breakup and collisions
- Conclusions



Major Physical and Chemical Mechanisms





Aluminized Propellants have both Gaseous and Condensed Phase Combustion Products

AP/binder flame is thin at propellant surface, while aluminum agglomerates are entrained into combustion gas and burn relatively slow

AP/Binder combustion products gas w/ entrained aluminum agglomerates



Solid Propellant











Surface Combustion Modeling Assumptions





Droplet Propellant Boundary

- Aluminum ignites ~2300 K
- Aluminum agglomerates at propellant surface
 - Pocket model
 - Measured size distribution



Turbulent Fluid Dynamics

Low-Re two equation (k- ϵ) model

Model Highlights

Captures transition from laminar to turbulent flow

Captures transition from 'inlet' to 'blowing wall'







Discrete Droplet Tracking

Lagrangian models assume dilute particle loading





Aluminum Droplet Combustion

Droplet rapidly approaches boiling pt of AI during burn

1-step Al burn rate (Hermsen, 1981) (Widener & Beckstead, 1998)





Aluminum Particle Burn Rate

1-step models account for oxide cap effects

Modified Hermsen

$$\frac{D}{D_0} = \left[1 - \frac{kt}{D_0^{1.8}}\right]^{\frac{1}{1.8}}$$

$$k = f\left(Y_{products}, P, Sh\right)$$

Tuned to lab experiments and adjusted for solid rocket motor data



Gas-Phase Combustion Modeling

As aluminum droplet burns, equilibrium with remaining gas is assumed

Elemental aluminum mass fraction transport equation $\frac{\partial(\rho Y_k)}{\partial t} + \nabla \cdot \left(\rho \vec{U} Y_k\right) = \nabla \cdot \left(\rho D \nabla Y_k\right) + \sum_i \alpha_{ki} m_{vi}$

Tabular data for gas-phase composition vs AI mass fraction and enthalpy





Droplet Breakup Results from High Speed Shear as Droplets Enter Nozzle

Breakup is controlled by the critical droplet Weber number

$$We_{c} = \frac{\rho \left| U_{R} \right|^{2} D_{P}}{\sigma_{P}}$$





Droplet Collisions

- Neglect large particle collisions
- Agglomeration due to collision of smoke particles
- "sweeping" model with collection efficiency





CFD Code Application

Super BATES test motor with 15% aluminum in solid propellant



*Sabnis, J.S.., "Numerical Simulation of Distributed Combustion in Solid Rocket Motors with Metalized Propellant, J. of Prop. & Power, 19(1), 2003."



Predicted Motor Pressure and Temperature

Distributed combustion (finite AI burn rate) shows temperature to be nonuniform



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Aluminum Mass Fraction and Density

94.3% of aluminum burns out before exiting nozzle





Conclusions

- Two-phase, distributed combustion model for metallized propellants was developed and applied
- Results of model show ability to simulate distributed combustion of aluminum in solid rocket motors
- CFD model provides a more sophisticated tool for solid rocket internal flow predictions
- CFD model still requires information regarding particle size distributions at propellant surface and fraction of metal that burns at propellant surface
- Application of the CFD model has been demonstrated, but validation of the model against carefully controlled experimental data would be nice
 - Will probably never happen
 - Must rely on post-test analyses of material response