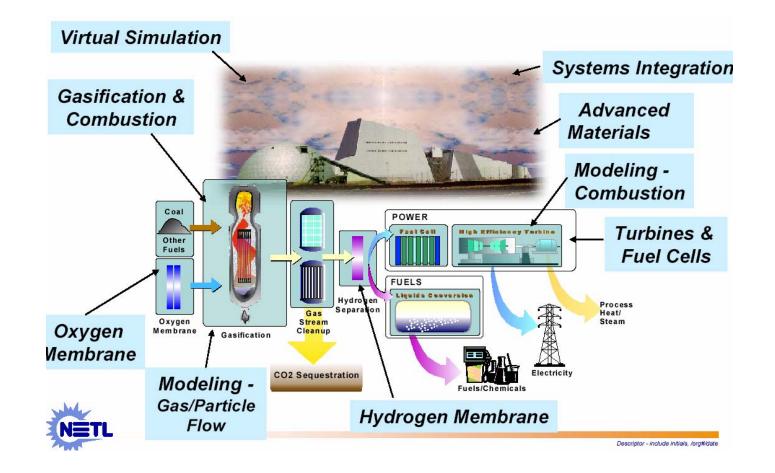
Modeling of Black Liquor Gasification in a Bubbling Fluidized Bed

REACTION ENGINEERING INTERNATIONAL

Biomass Utilization Workshop February 10, 2004

Gasification of Solid Fuels



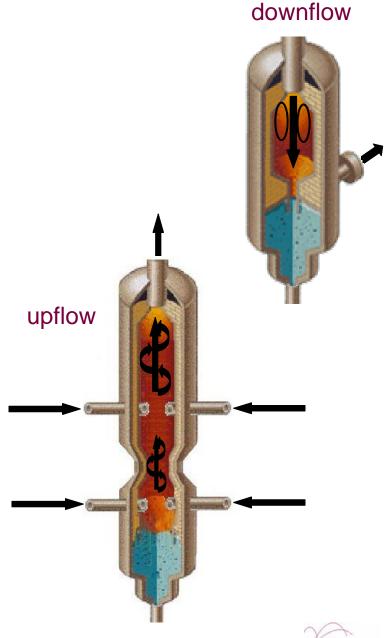


Entrained Flow Gasifier Model

- Model Development
 - Configurations:
 - » downflow / upflow
 - » 1 stage / 2 stage
 - » based on public information
 - Parameters
 - » Process conditions, burner characteristics
 - » Fuel type, slurry composition
 - » gross geometry
 - Submodel developments
 - » high pressure gasification reaction kinetics
 - » slag, ash, soot, tar
 - » air toxics (metals, PM2.5)

Collaborations

- EPRI
- Black Coal CCSD, Australia
- IVD, U. of Stuttgart



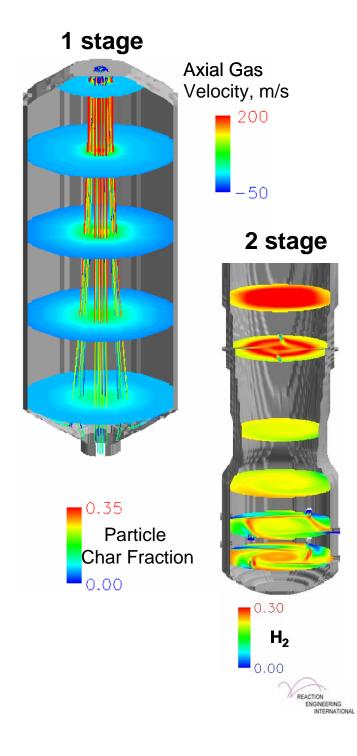


Gasifier - CFD Model

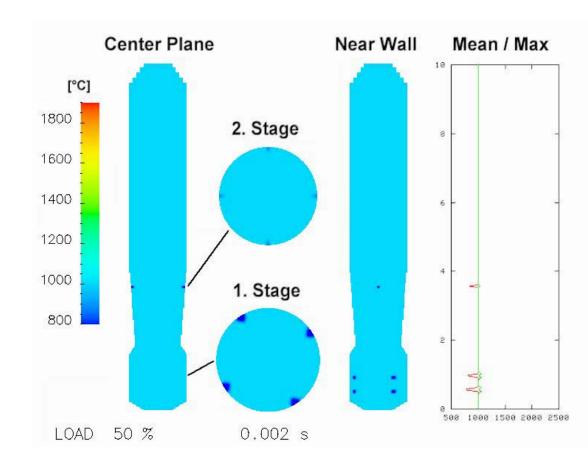
- 1 & 2 stage gasifier designs
- provides details on
 - gas flow field
 - » temperature, velocity, species
 - wall conditions:
 - » temperature, heat flux
 - » critical viscosity, slag flow
 - carbon conversion, cold gas efficiency
 - unburned carbon in slag and flyash
 - generated syngas
 - » speciation, temperature, particle loading,...
- evaluate impact on
 - carbon conversion, syngas, slag and ash properties, refractory

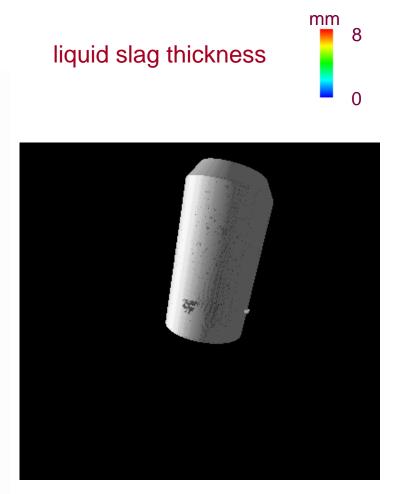
due to:

- fuel change or co-firing:
 - » coal / char-recycle / petcoke / waste / biomass
- oxidant: oxygen concentration, pre-heat
- feed: wet vs dry, solids loading, pre-heat



Detailed Results





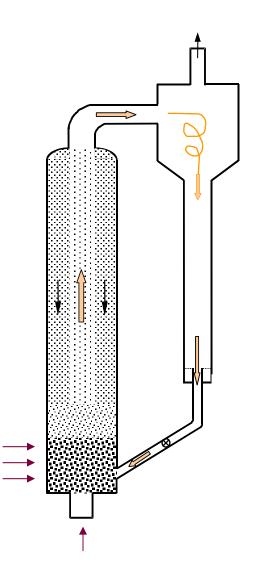


Gasifier – Transport Reactor

- ➔ 1.5D, CFB, core/annulus engineering model
- Provides elevation profiles for
 - gas flow field
 - » temperature, velocity, species
 - wall conditions
 - » temperature, heat flux
 - solids
 - » carbon conversion, particle size
 - » coal, char, limestone, sand
- Overall estimates for
 - cold gas efficiency
 - syngas: speciation, temperature, particle loading
 - solids/particles: size distribution, carbon conversion
- evaluate impact on
 - carbon conversion, syngas quality, particle size, refractory

due to:

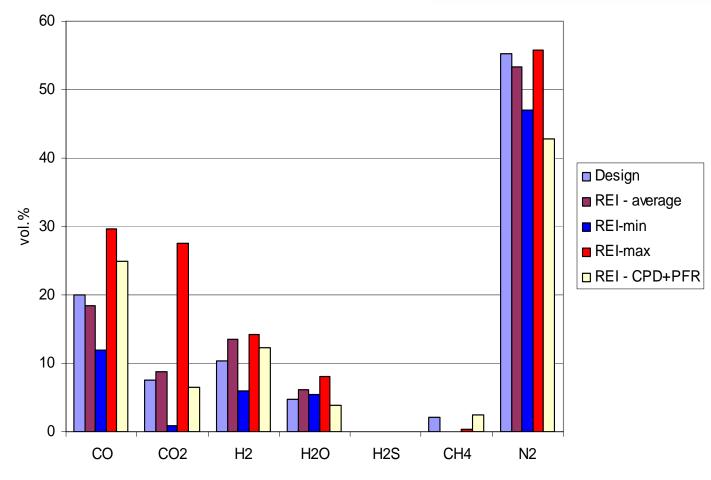
- fuels: coal / petcoke / waste / biomass / char
- oxidizer: air, oxygen blown/enriched, pre-heat
- ♦ FGR
- solids: grind, drying, pre-heat





Syngas Composition Predictions

Fueltype	Powder River Basin, Alabama Calumet Bituminous
Fuel particle size, µm	200 - 350
Fuel feed rate, pph	2700 - 5000
Sorbent type	Ohio Bucyrus limestone
Sorbent particle size, µm	10 - 30
Sorbent feed rate, pph	0 - 200
Reactor temperature, °F	1670 - 1825
Reactor pressure, psig	140 - 240
Riser gas velocity, fps	40 - 60
Riser mass flux, lb/ft ² s	150 - 700
Air/coal mass ratio	2.5 - 3.5
Steam/coal mass ratio	0.0 - 1.0





Fluidized Bed Gasification of Black Liquor

A key DOE/Georgia Pacific supported technology option (MTCI) being demonstrated at Big Island, VA

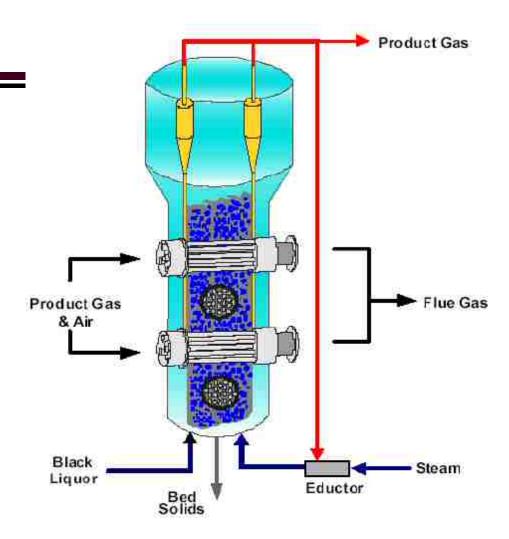
→ Features:

- bubbling bed
- high efficiency & chemical recovery
- improved emissions
- lower maintenance costs
- elimination of smelt/water explosion hazard
- Modeling Objectives:
 - describe impact of design conditions and operating conditions
 - support troubleshooting with pilot and demonstration units



MTCI Specifics

- Steam reforming process operating in the bubbling regime
- Design capacity of 180 tons/day
- Design incorporates 4 tube bundles (pulse combustors) with 253 horizontal tubes each, arranged in a staggered configuration



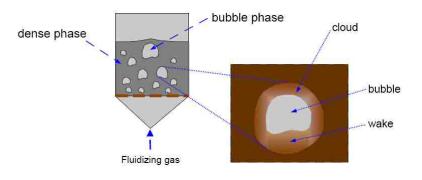


Model Approach

- Three phase counter-current with back mixing
 - particle free bubble phase
 - wake-cloud phase
 - dense particle phase



- Particle temperatures in different phases are treated separately
- Bubble size and velocity determined using standard correlations such that:
 - bubbles grow with height
 - bubbles break up in tube banks
- Bubbles play a major role in driving solids circulation in bed impacting temperature distribution, concentration profiles, and bed agglomeration





Particle Models

Devolatilization

- Empirical correlations are used to determine C, H, O and S release (Frederick and Hupa, 1993; Frederick et al., 1995)
- Volatiles are represented by a mixture of CH₄, CO, H₂O and H₂S

 $C_aH_bO_cS_d = eCH_4 + fCO + gH_2O + hH_2S$

Amount of each gas species released is determined from the element mass balance

Gasification Kinetics

Steam gasification (Li and van Heiningen, 1991; Wessel et al., 1997)

 $C + H_2O = CO + H_2$ Rate = 2.56×10⁹ exp $\left(-\frac{25300}{T_p}\right)\frac{P_{H_2O}}{P_{H_2O} + 1.42p_{H_2}}C_e$ kmol/m³s

CO₂ gasification (Li and van Heiningen, 1990; Wessel et al., 1997)

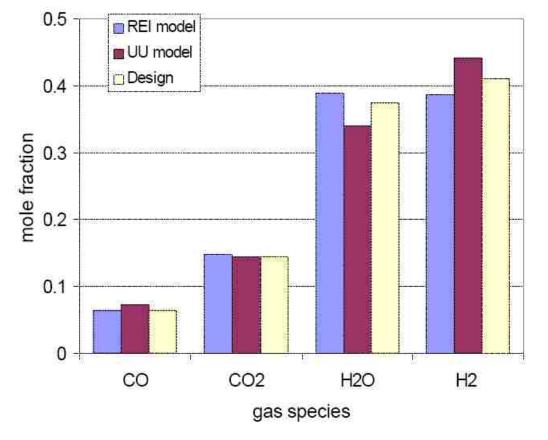
C+CO₂ = 2CO Rate = $6.30 \times 10^{10} \exp\left(-\frac{30070}{T_0}\right) \frac{P_{CO_2}}{P_{CO_2} + 3.4 P_{CO}} C_c$ kmol/m³s

Other reactions considered

$$\begin{array}{lll} CH_4 + H_2O = CO + 3H_2 & CH_4 + 2O_2 = CO_2 + 2H_2O \\ C + 2H_2 = CH_4 & H_2 + \frac{1}{2}O_2 = H_2O \\ C + \frac{1}{2}O_2 = CO & CO + H_2O \leftrightarrow H_2 + CO_2 \\ CO + \frac{1}{2}O_2 = CO_2 & \end{array}$$



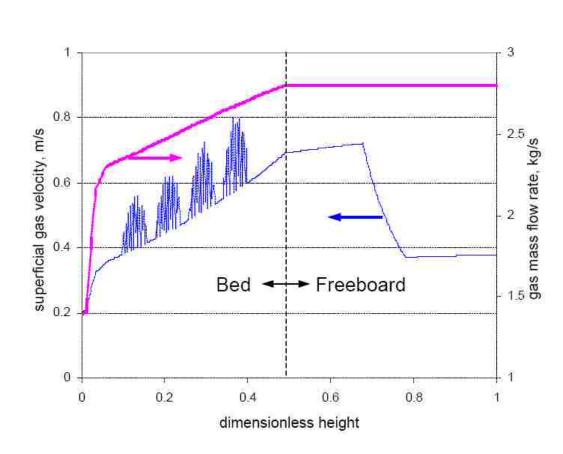
Model Results: Syngas Composition



- Model predictions very similar to those of Whitty 2003, based on 10 zones with equal gasification
- Georgia Pacific reports carbon conversion of 95%, while model predicts 99.6%



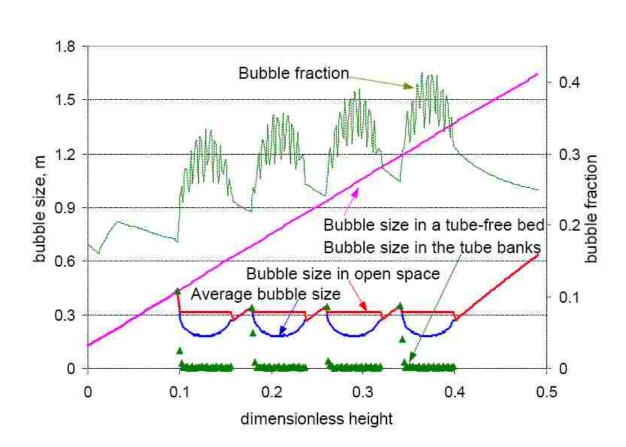
Model Results: Gas Velocity & Mass Flow Rate



- Jump increases in both gas mass flow rate and the gas velocity due to moisture vaporization and black liquor pyrolysis
- Spikes in gas velocity inside tube bundles due to changes in cross sectional area of the bed



Model Results: Bubble Size and Fraction

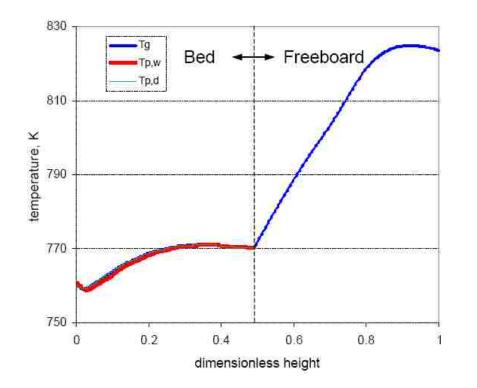


Variation of bubble properties with bed height

- Inside the tube bundles, bubble size is similar to the tube pitch
- Bubble fraction ranges from 0.15 to 0.40, where spikes in the tube bank are due to gas velocity increase
- An area-averaged bubble size is used in the model



Model Results: Gas and Particle Temperatures

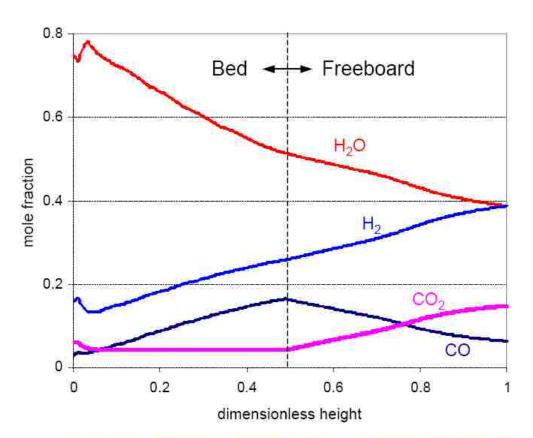


Gas temperature and particle temperature as functions of reactor height

- Particle temperatures very close to gas temperatures
- Vaporization of water near bottom leads to a decrease in temperature, followed by an increase resulting from heat transferred from the pulse combustors
- In the freeboard, there are two major reactions:
 - exothermic water-gas shift
 - endothermic methanewater reforming



Model Results: Gas Composition



Variation of gas composition with reactor height

- As gasification proceeds, water vapor decreases and CO and hydrogen increases
- In the freeboard, hydrogen and CO2 increase while water vapor and CO decrease
- methane-water reforming is minimal due to low methane concentration

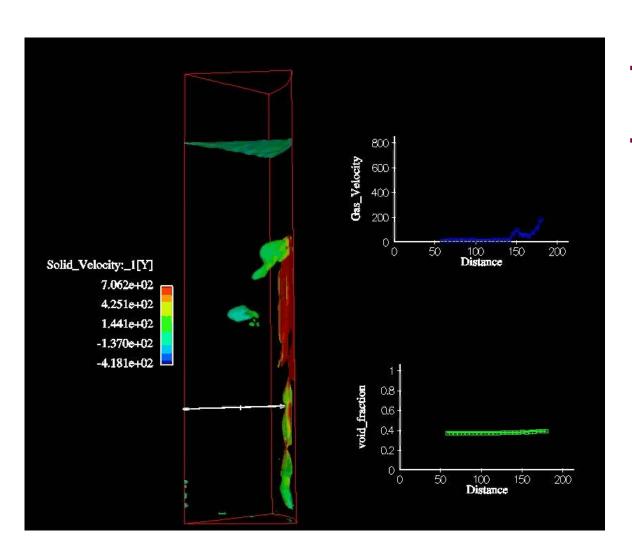


Model State and Development

- → Currently
 - The three-phase model provides estimates of syngas concentrations and carbon conversion consistent with the limited data
 - Gas and particle temperature profiles, important for tar formation and bed agglomeration
- → Upcoming
 - Further validation of the model will be carried out as experimental data become available
 - Effects of operating conditions on the performance of the gasifier will be performed



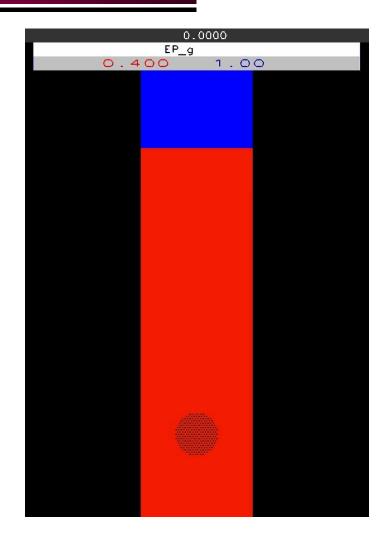
CFD Modeling of FB BLG



- Collaboration with Rand Batchelder
- MFIX code developed at NETL
- Potential for improvements in predictions and evaluation of 3D and transient phenomena



Injector Effects





Tube Bundle Interactions

